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Full Length Research Paper

Experimentally Characterization of Coated Cutting Tools Life with Applications to Dies Materials

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The objectives of this study were to investigate the possibility of optimizing the cutting performance for dies materials machining process from hard steel using different coated Cobalt-cemented tungsten carbide (WC-Co) tool inserts (substrates) for finish turning carbon steel (AISI D2). In addition, comparison between uncoated and coated inserts was performed depending on machining speed, feed, and cutting depth without cooling fluids. Chips types and work piece surface roughness were also studied. As a result we were able to increase cutting tool life which will influence the machining process cost

Keywords: Cutting tools, Dies forming, hardest conditions, Manufacturing.

INTRODUCTION

Increasing demands for high speed and high performance dry machining applications have brought new challenges for the quality of cutting tool materials. High performance dry machining generates severe cutting conditions associated with high temperature and stress within the cutting zone.

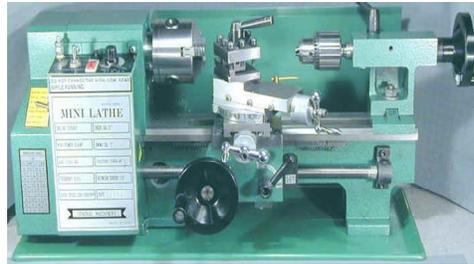
In this application of machining hard materials for dies manufacturing in Jordan the use of advanced coated tools is critical to realizing the benefits of high performance machining. Traditional hard coatings, such as titanium-nitrides (Ti-N) single layer coatings, played an important role in the development stage of new-generation cutting tools in an attempt to improve the wear resistance of cutting and forming tools (Mills and Redford, 1983 : Geoffrey, 1975). A major drawback of Ti-N, however, is its limited resistance to oxidation at high temperatures that can be reached during different cutting processes. For this reason, high-temperature chemical stability is a major prerequisite for hard coatings (Ostwald and Phillip, 1996).

Recent improvements in the coatings of cutting tools have been achieved by the development of (Ti-Al) N coatings. (Ti-Al) N coatings exhibit good wear resistance, high oxidation resistance, high hardness at elevated temperatures, thermal and chemical stability, and low thermal conductivity (Nargpal, 1996 : Shaw, 1984 : Rajender, 2006 : Hugh, 2001). An extremely important advantage of (Ti- Al) N coatings is that it possesses a high thermal stability due to the formation of a dense, highly adhesive, protective Al₂O₃ surface film on the (Ti-Al) N coating in the process of cutting. Such a film prevents diffusion of oxygen into the coating and thus reduces the diffusion wear, one of the major wear mechanisms in cutting tools (McIntyre et al., 1990 : Han et al., 1996 : Wang, 1997 : Wang et al., 1999 : Kimura et al., 2006 : Kimura et al., 2001 : Prengel et al., 1997). For this reason (Ti-Al)N has become one of the best solutions as coating material for cutting tools, especially for dry and high speed cutting.

In the current study Metal cutting or traditional

Table 1. Chemical Composition of steel (AISI D2) workpiece material .

C%	Si%	Mn%	Cr%	S%	V%
1.55	0.3	0.4	11.8	W	0.8

**Figure 1.** The specification of lath machine name (Ferdinand cribber).**Table 2.** Specifications of Centre Lathe Machine used in Experimental Tests

Spindle speed	Feed rate	Total power
22– 2400 (r.p.m)	0.08 - 6.4 mm/rev.	6.6 KW for 50 Hz

machining processes (conventional machining processes) were carried on hard die steel materials using different coated Cobalt-cemented tungsten carbide (WC–Co) tool inserts (substrates) for finish turning carbon steel Machining tests were carried out on a quenched-tempered steel (AISI D2). In addition, comparison between uncoated and coated inserts was performed depending on machining speed, feed, and cutting depth without cooling fluids. Chips types and workpiece surface roughness were also studied. As a result we were able to increase cutting tool life which will influence the machining process cost. SEM were used to measure the cutting tool life and wear of each sample after test.

Experiment set

Tests were conducted on some specimen of materials made from quenched-tempered Cr4.2Mo4 steel (DIN 1.7225 / SAE 4140). Which is used widely in several industrial products specially dies industry in Jordan for several applications such as plastic dies, aluminum extrusion dies and many other applications. Die materials hardness was measured as 55 HRC . Table 1 shows the chemical compositions of die metals. While Fig .1 and table 2 show the specification of lath machine name (Ferdinand Cwibert) Fig 2. Shows work piece and its dimensions (inside diameter 195 mm and outside 207 mm).

Four different cutting tools with different specifications are used, each have been utilized according to certain conditions of cutting operations as follows:

- Depth of cut (mm).
- Feed rate (mm/rev).
- Cooling liquid.

- Cutting speed (m/min).
- Automatic feed rate.

Cutting operation

A lathe machine is used on one of the edges of specimen No.1 along with 1mm cutting depth, 0.1 mm/rev feed rate, 23 m/min speed of cutting and without any cooling liquids which represents the hardest conditions.

In the second time, another edge for the same specimen along with 1mm cutting depth, 0.1 mm/rev feed rate, 29 m/min speed of cutting and without cooling liquid are used.

In the third time, we used another edge for the same specimen along with 0.5mm cutting depth, 0.1 mm/rev feed rate, 23 m/min speed of cutting and without cooling liquid.

In the last, we used another edge for the same specimen along with 0.5mm cutting depth, 0.1 mm/rev feed rate, 29 m/min speed of cutting and without cooling liquid.

In these experiments, the feed rate was completely automatic, and traveled distances for each cutting tool edge was 150 m. Specimen No.2 was implanted but no cutting happened.

The same procedures are repeated for specimen No.3 and No.4 and the following results were obtained as in table 3.

Surface roughness

After each experiment is done, measure the roughness of the surface being cut using a special purpose roller (flex

Table 3. Edge number, kind of chip with cutting speeds and depth of cut.

		T1		T2	T3		T4	
		Chips	edge number		chips	edge number	chips	edge number
edge one	depth of cut = 0.5 (mm) speed of cut = 29 (m/min)	1	 2	no cutting happened	4	 1A	8	 1A
edge two	depth of cut = 0.5 (mm) speed of cut = 23 (m/min)	1	 3		6	 08	10	 02
edge three	depth of cut = 1 (mm) speed of cut = 23 (m/min)	3	 3		7	 08	11	 1A
edge four	depth of cut = 1 (mm) speed of cut = 29 (m/min)	2	 2		5	 1A	9	 02



Figure 2. photo of workpiece test sample.



Figure 3. photo of machining tool No.1 during cutting process



Figure 4. photo of machining tool No.2 during cutting process



Figure 5: photo of machining tool No.3 during cutting process



Figure 6: photo of machining tool No.4 during cutting process

Table 4. Surface Roughness values at different machining conditions for tools with coated inserts.

Feed rate (mm/rev)		0.1				0.1			
Depth of cut(mm)		0.5				1			
Tool No*		T1	T2	T3	T4	T1	T2	T3	T4
		Surface roughness(Ra) (µm)							
Cutting speed m/min	23	3.4	-----	1.6	2.8	6.3	-----	3.6	5
	29	3.2	-----	1.4	2.6	6	-----	3.5	4.8

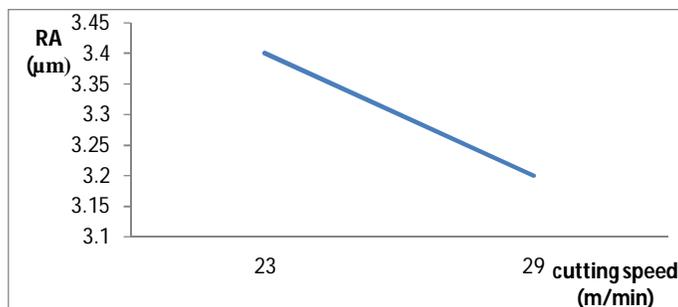


Figure 7. cutting speed [m/min] vs surface roughness [µm].

Table (5). wear length in different edges of cutting tool.

	T1		T2	T3		T4	
	edge	wear length (µm*10 ³)		edge	wear length (µm*10 ³)	edge	wear length (µm*10 ³)
depth of cut = 1 (mm) speed of cut = 23 (m/min)	2	0.79	No measurements were taken	0 8	0.69	A 1	1.27
depth of cut = 1 (mm) speed of cut = 29 (m/min)	3	0.83		A 1	0.8	0 2	1.44
depth of cut = 0.5 (mm) speed of cut = 23 (m/min)	2	0.42		0 8	0.33	0 2	0.95
depth of cut = 0.5 (mm) speed of cut = 29 (m/min)	3	0.48		A 1	0.38	A 1	0.98

bar no. 16008) was used .the results are shown in table 4.

Fig. 7 below shows the relationship between cutting speed [m/min] and surface roughness [µm].

Examining cutting tools wear

In this step each edge wear after finishing the cutting using digital micrometer is measured and the results are shown in table 5.

Fig. 8 to 10 shows a comparison between the cutting tools with respect to the wear length and cutting depth relation, it can be noticed that tool number four has the maximum wear length while number three has a minimum one.

Chip formation

The examining tool gives different types of chips given in table 6.

RESULTS AND DISCUSSION

It is figured out – from the reading that have been took during cutting – that there is a noticeable difference between each cutting tool regarding the following items: shape of formed surface , shape of chips and the wear done on each tool , and there is a difference between each edge for the same cutting tool depending on various conditions (Figures (11-13) shows SEM photose of some of the samples with sever wear.

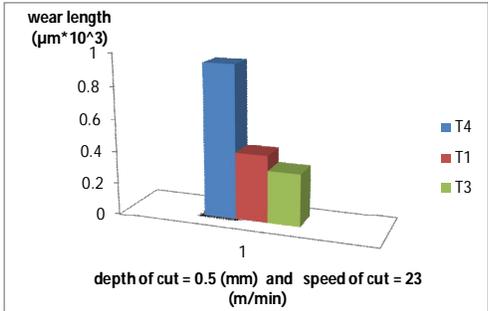
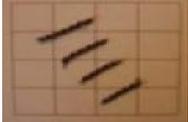


Fig. 8: wear length ($\mu\text{m} \cdot 10^3$) vs depth of cut = 0.5 (mm) and speed of cut = 23 (m/min)

Table 6. types of formed chip

Number of chips	Type of chips	form of chips
1	2	
4	6	
7	11	
8	Short helical Broken chips	
10	Medium helical Broken chips	
3	Long helical Broken chips	
9	Long helical Unbroken chips	
5	Long and snarled Unbroken chips	

Cutting Tool No.1

When applying depth of cut 0.5 mm along with 23 m/min , we have come out with $R_a=3.4 \mu\text{m}$ but when applying 29 m/min with depth of cut remain the same , we have come out with $R_a=3.2 \mu\text{m}$.This lead us to a simple conclusion; that when we increase speed of cut, surface roughness decrease. For the same parameters we get short helical broken chips and c-type/3-type broken chips, respectively. This shows us that when we increase speed of cut, we get the desired chips. When applying depth of cut 0.5 mm along with 23 m/min, we have come out with wear length= $(0.42 \mu\text{m} \cdot 10^3)$ but when applying 29

m/min with depth of cut remain the same, we have come out with wear length= $(0.48 \mu\text{m} \cdot 10^3)$.This lead us to a simple conclusion; that when we increase speed of cut, wear length increases. When applying depth of cut 1.0 mm along with 23 m/min , we have come out with $R_a=6.3 \mu\text{m}$ but when applying 29 m/min with depth of cut remain the same , we have come out with $R_a=6.0 \mu\text{m}$.This lead us to a simple conclusion; that when we increase speed of cut, surface roughness decrease. For the same parameters we get long helical broken chips and c-type/3-type broken chips, respectively. This shows us that when we increase speed of cut, we get the desired chips. When applying depth of cut 1.0 mm along with 23

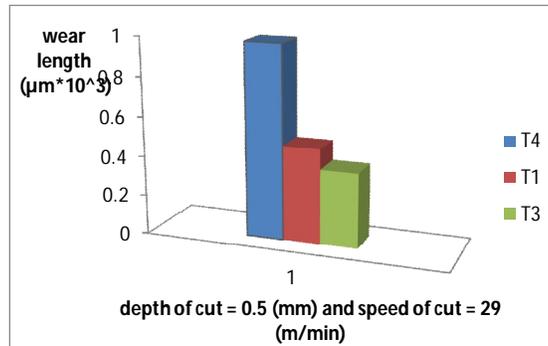


Figure 9: wear length (µm*10³) vs depth of cut = 0.5 (mm) and speed of cut =29(m/min)

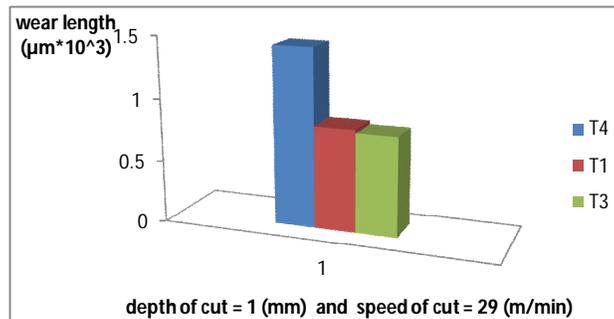


Fig 10: wear length (µm*10³) vs depth of cut = 1 (mm) and speed of cut =29(m/min)

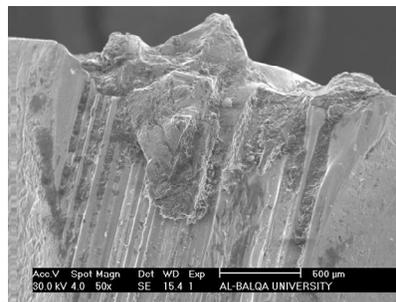


Figure 11 SEM images of coated tool inserts No.3 after machining at 29 m min⁻¹

m/min, we have come out with wear length= (0.79 µm*10³) but when applying 29 m/min with depth of cut remain the same, we have come out with wear length= (0.83 µm*10³).This lead us to a simple conclusion; that when we increase speed of cut, wear length increases.

Cutting Tool No.2

Slight ignorant cutting is done, no measurements were taken.

Cutting Tool No.3

When applying depth of cut 0.5 mm along with 23 m/min ,

we have come out with Ra=1.6 µm but when applying 29 m/min with depth of cut remain the same , we have come out with Ra =1.4 µm .This lead us to a simple conclusion; that when we increase speed of cut, surface roughness decrease. For the same parameters we get short helical broken chips and c-type/3-type broken chips, respectively. This shows us that when we increase speed of cut, we get the desired chips. When applying depth of cut 0.5 mm along with 23 m/min, we have come out with wear length= (0.33 µm*10³) but when applying 29 m/min with depth of cut remain the same, we have come out with wear length= (0.38 µm*10³).This lead us to a simple conclusion; that when we increase speed of cut, wear length increases. When applying depth of cut 1.0 mm along with 23 m/min , we have come out with Ra=3.6 µm but when applying 29 m/min with depth of cut remain

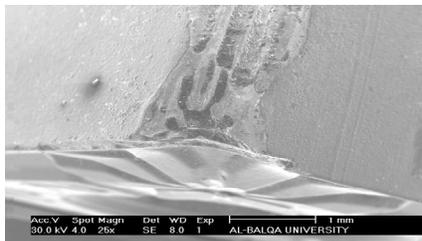


Figure 12. SEM images of coated tool inserts No.1 after machining at 29 m/min

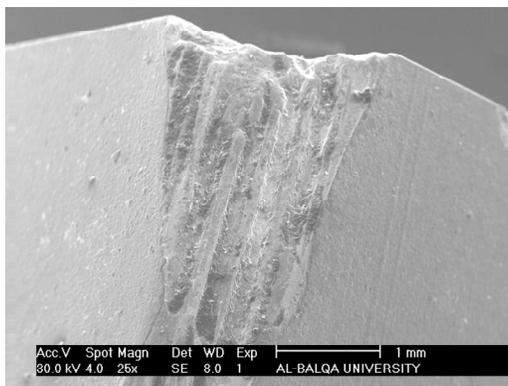


Figure 13 SEM images of coated tool inserts No.4 after machining at 29 m/min

the same, we have come out with $Ra = 3.5 \mu\text{m}$. This leads us to a simple conclusion; that when we increase speed of cut, surface roughness decreases. For the same parameters we get long and snarled unbroken chips and c-type/3-type broken chips, respectively. This shows us that when speed of cut is increased, the desired chips are formed. Generally, unbroken long chips are not desired. When applying depth of cut 1.0 mm along with 23 m/min, we have come out with wear length = $(0.69 \mu\text{m} \cdot 10^3)$ but when applying 29 m/min with depth of cut remain the same, the wear length will be = $(0.80 \mu\text{m} \cdot 10^3)$. This leads us to a simple conclusion; that when we increase speed of cut, wear length increases.

Cutting Tool No.4

When applying depth of cut 0.5 mm along with 23 m/min, we have come out with $Ra = 2.8 \mu\text{m}$ but when applying 29 m/min with depth of cut remain the same, we have come out with $Ra = 2.6 \mu\text{m}$. This leads us to a simple conclusion; that when we increase speed of cut, surface roughness decreases. For the same parameters we get medium helical broken chips and short helical broken chips, respectively. This shows us that when we increase speed of cut, we get the desired chips. When applying depth of cut 0.5 mm along with 23 m/min, we have come out with wear length = $(0.95 \mu\text{m} \cdot 10^3)$ but when applying 29 m/min with depth of cut remain the same, we have come out with wear length = $(0.98 \mu\text{m} \cdot 10^3)$. This leads us to a

simple conclusion; that when we increase speed of cut, wear length increases. When applying depth of cut 1.0 mm along with 23 m/min, we have come out with $Ra = 5.0 \mu\text{m}$ but when applying 29 m/min with depth of cut remain the same, we have come out with $Ra = 4.8 \mu\text{m}$. This leads us to a simple conclusion; that when we increase speed of cut, surface roughness decreases. For the same parameters we get long helical unbroken chips and c-type/3-type broken chips, respectively. This shows us that when we increase speed of cut, we get the desired chips. Generally, unbroken long chips are not desired. When applying depth of cut 1.0 mm along with 23 m/min, we have come out with wear length = $(1.27 \mu\text{m} \cdot 10^3)$ but when applying 29 m/min with depth of cut remain the same, we have come out with wear length = $(1.44 \mu\text{m} \cdot 10^3)$. This leads us to a simple conclusion; that when we increase speed of cut, wear length increases.

CONCLUSION

The discussions of the best cutting tool have been made by examining a number of inserts under specific conditions and we get the following conclusion:

Cutting tool NO.1

a- It has the highest surface roughness in all cases that, depth of cut 0.5 mm and speed of cut 23 m/min. And

the highest surface roughness at depth of cut 1mm and speed of 29 m/min.

b- It has a medium wear length.

Cutting tool NO.2

There is no cutting happened so it is very highly wear because it is coated by a layer of carbon that has a low friction coefficient.

Cutting tool NO.3

a- It has the lowest surface roughness in depth of cut 0.5 mm and speed of cut 23 m/min .And the highest surface roughness at depth of cut 1mm and speed of 29 m/min.

b- It has a lowest wear length.

Cutting tool NO4

a- It has the medium surface roughness in all cases that, depth of cut 0.5 mm and speed of cut 23 m/min .And the highest surface roughness at depth of cut 1mm and speed of 29 m/min.

b- It has a lowest wear length.

5-the uses of a specific kind of cutting tool depends on the application of the products like surface roughness of theme and the hardness of metal used.

6-coating the cutting tools improve theme; it becomes higher thermal resistance, long life, higher wear resistance and higher mechanical characteristic.

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